

CAPACITOR BANKS SELECTION IN RADIAL DISTRIBUTION NETWORKS BY COMBINED ALGORITHM

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This paper presents the combined algorithm for determination of locations and sizes of capacitor banks in the radial distribution networks for practical minimization of power losses and costs of these losses and banks. The method of concessions and modified PSO-method are applied in the proposed algorithm. Additionally the technicalcoenosis criterion is applied for the specific account of technical and economic factors. The proposed approach allows to obtain the efficient practical solutions and increased stabilization of voltage profile in the radial distribution network.

References 9, tables 4, figures 2.

Keywords: capacitor bank, combined algorithm, radial distribution network, method of concessions, PSO-method, technicalcoenosis criterion.

I. Introduction. A significant part of active power losses in radial distribution networks (RDN) occurs due to the flow of reactive currents and therefore the application of capacitor banks (CB) for reactive power compensation is very important.

In this paper, the combined algorithm of CB selection (sizing and placement in distribution network) is developed as a combination of traditional optimization criteria, i.e. power losses and investment cost minimization, and additional technical-coenosis criterion. Also the method of concessions and modified particle swarm optimization (PSO) method are applied.

The comprehensive survey of the literature from the last decade that has focused on the various heuristic optimization techniques applied to CB selection in RDN was presented in [6]. This analysis of published papers shows that PSO is the most popular technique applied because of its advantages, which include simple implementation, small computational load and fast convergence.

II. Problem description and solution method. Two main criteria for CB placement and sizing are usually considered as the following two objective functions used to minimize yearly active losses and costs

of these losses and shunt CB installation
$$\Delta P_{\Sigma} = \sum_{i=1}^q \Delta P_i \rightarrow \min, \quad (1)$$

where ΔP_{Σ} – total active power losses and $\sum_{i=1}^n \Delta P_i$ – losses in the i section/node distribution system, q –

number of nodes.
$$B_{\min} = K_p \Delta P_{\Sigma} + \sum_{i=1}^{nc} K_{ci} Q_{ci} \rightarrow \min, \quad (2)$$

where K_p – annual cost per unit of active losses ΔP_{Σ} (\$/(kW*year)), K_{ci} – annual cost of reactive power Q_{ci} corresponding i -th CB (\$/(kVAr*year)), nc – total number of CB to be installed.

The function (1) may have many constraints, but in this paper we are considering only one of them, which is the voltage profile constraint: voltage magnitude at each node must be maintained within the limits:

$$U_{\min} \leq |U_i| \leq U_{\max}, \quad (3)$$

where U_{\min} , U_{\max} – minimum and maximum permissible voltage.

The analysis of problem solutions by using only traditional criteria (1) and (2) shows that they do not always give a positive result in the presence of such circumstances as inadequate pricing in conditions of economic crises, the technical information imprecision, specific features of the networks requirements and sometimes in terms of engineering logic. In these conditions the additional criteria, approaches and analysis methods should be applied.

III. Solution algorithm. In order to overcome the above mentioned problems in this paper the application of well-known method of concessions is proposed. It allows to find theoretically only the quasi-

optimal solution, which can be interpreted as rational and efficient for practical purposes. For the objective function minimum value can be assigned the concession δ , %, as its permissible decline for practical purposes, accuracy requirements etc.

The proposed algorithm for solving the CB selection problem consists of the following procedures.

1. According to the results of PSO procedures application, for each swarm particle m the vector of n CB (in the nodes of RDN) conductivities \mathbf{y}_1 is formed. The basic set of solutions \mathbf{Y}_1 is formed by these vectors \mathbf{y}_1 by criterion (1) with constraint (3). The set of solutions \mathbf{Y}_1 is formed of \mathbf{y}_1 vectors, which are in the range of allowable concession δ_1 of minimum losses in RDN

$$\mathbf{y}_1(y_1, y_2, \dots, y_n) : \Delta P_{\Sigma}(y_1, y_2, \dots, y_n) \leq (1 + \delta_1) \Delta P_{\Sigma \min}.$$

2. From the solutions set \mathbf{Y}_1 we form another set of solutions $\mathbf{Y}_2 \subset \mathbf{Y}_1$, which is composed of vectors \mathbf{y}_2 by criterion (2) and its allowable concession δ_2

$$\mathbf{y}_2(y_1, y_2, \dots, y_n) : B(y_1, y_2, \dots, y_n) \leq (1 + \delta_2) B_{\min}.$$

The set \mathbf{Y}_2 also can be defined by PSO-method separately from the set \mathbf{Y}_1 . The resulting set can be defined as the intersections of corresponding solution sets

$$\mathbf{Y}'_2 = \mathbf{Y}_1 \cap \mathbf{Y}_2 \neq \emptyset.$$

In the case of empty set \emptyset the allowable concessions δ_1, δ_2 then sequentially have to be changed and calculations of \mathbf{Y}_2 or \mathbf{Y}'_2 have to be repeated.

3. From the set \mathbf{Y}_2 (or \mathbf{Y}'_2 , in case when intersection method is applied) we choose the best solution by additionally applied the Technical-coenosis (TC) criterion. This criterion establish the conformity of ranged values of CB conductivities to hyperbolic (power law) H -distribution [4] from the set of solutions $\mathbf{Y}_{TC} \subset \mathbf{Y}_2$. According to TC-approach the electrotechnical systems can be considered as TC [4], where a certain "family" of electrical products (for example CB in our case) can be arranged by particular species-forming parameters [2,4]

$$C(r) = C_1 / r^\beta, r = 1, 2, \dots, d, \quad (4)$$

where r – parametric rank; C_1 – parameter value of individual with a rank $r = 1$; β – rank factor characterizing the degree of curve distribution steepness, d – total number of ranks.

The values of the first rank and rank factor are very important, since together they define the range of CB in RDN and their quantity: $C_1 \rightarrow \min$ with the condition of the best approximation to hyperbola with $0,5 \leq \beta \leq 1,5$, which corresponds to highly effective state of TC [2,4]. At the same time, to determine the most acceptable H -distribution of the first rank and rank factor we can apply the concession δ_3 for C_1 parameter.

The additional TC-criterion for vector of CB conductivities $\mathbf{y}(y_1, y_2, \dots, y_n)$ have to be defined by (5) for the following conditions:

– similarity of normalized target vector \mathbf{y} to normalized vector in the form of a hyperbolic dependence;

– minimization of the magnitude of CB conductivity of the first rank $\mathbf{y}_{(r=1)}$.

$$\left\{ \begin{array}{l} y_{TC}^{nor}(r) = y_{TC(r=1)}^{nor} / r^\beta \\ d_E(\mathbf{y}_{TC}^{nor}, \mathbf{y}_{rank}^{nor}) < \delta_3 \\ y_{TC(r=1)}^{nor} \rightarrow \min, \end{array} \right. \quad (5)$$

where $d_E(\mathbf{y}_{TC}^{nor}, \mathbf{y}_{rank}^{nor})$ – the Euclidean distance between normalized vectors, δ_3 – permissible concessions of the distance between normalized vectors, vector \mathbf{y}_{rank}^{nor} – vector \mathbf{y}^{nor} after ranking, $\mathbf{y}_{rank}^{nor} = \text{sort}(\mathbf{y}^{nor}, \text{descend})$, operator 'sort' sorting vector \mathbf{y}^{nor} in the order specified by mode, mode 'descend' indicates descending order [5]. The unit length of normalized vectors is $|\mathbf{y}_{TC}^{nor}| = 1, |\mathbf{y}_{rang}^{nor}| = 1$. The concession δ_3 allows to estimate the similarity of searching vector \mathbf{y} to vector in the form of a hyperbolic dependence in accordance with TC-criterion.

It is known that in PSO-method each particle moves in the multi-dimensional set of solutions [1, 8]. Moreover, the particle position x_k is determined by the interaction with all other particles of swarm. All particles move to the global extremum; the process occurs at the end of the relevant performance of breakpoint criteria. One of the classical optimization algorithms of continuous nonlinear functions, named in [7] as “A modified particle swarm optimizer” is used in this paper. To calculate the position and velocity for n -dimension of m particles, the following expressions are used at each k iteration

$$V_{k+1} = \omega V_k + a_1 R(Pbest_k - x_k) + a_2 R(Gbest_k - x_k), \quad x_{k+1} = x_k + V_{k+1},$$

where x_k – current position of particle, V_k – particle velocity, a_1, a_2 – constants of acceleration, $Pbest$ – best position found by particle, $Gbest$ – best position found by all particles, ω – inertia factor, R – random number between 0 and 1.

The distinctive feature of this PSO-algorithm is the ability to control the speed of convergence process using the number of particles in the swarm and the inertia factor. After PSO-method modification, intermediate results of each iteration computation x_k are not discarded, but are grouped in the appropriate set of solutions. In addition, at the beginning of the process a suitable total number of particles and the ratio of inertia are chosen.

As a result of the modified PSO-method application, a corresponding set of solutions is formed. In this set, each m particle corresponds to the n -dimensional vector of CB conductivities $y(y_1, y_2, \dots, y_n)$ consisting of n CB, which has to be installed in the corresponding feeder nodes.

The application of criteria (1), (2), (4) and voltage profile constraint (3) with the method of concessions and modified PSO-method gives the combined algorithm of CB selection for radial distribution networks. The fixed CB capacities are defined by using the proposed algorithm for the regime of maximum load in RDN. For the determination of CB steps of regulation the daily schedules, controller switching codes, and other engineering methods have to be used.

IV. Test results. The proposed algorithm was used for CB selection in the radial network, with a rated voltage 23 kV, which consists of 27 nodes ($q=27$) and 21 loads ($n=21$), considered in [9]. Permissible voltage [0,95 – 1,05]. The calculation was carried out in the absence of harmonic current sources for a period of 8760 hours per year. The energy losses cost is taken as 0,06 \$/KW·h. Technical data of conductors are taken from [9]. The base values of power and voltage for calculations are the following: $S_b = 24$ MVA,

$U_b = 23$ kV. The types of wires were chosen previously and this procedure is not described in the example. The conductor selection problem, as it was done in some studies [3, 9], is not considered. The power values of CB are considered with discreteness 150 kVar. The CB j sizes (reactive power) Q (kVar) and accepted costs B_c \$/(kVar*year) are taken as presented in Table I.

j	1	2	3	4	5	6	7	8
Q	150	300	450	600	750	900	1050	1200
B_c	0,5	0,35	0,253	0,22	0,276	0,183	0,228	0,17
j	9	10	11	12	13	14	15	
Q	1350	1500	1650	1800	1950	2100	2250	
B_c	0,207	0,2	0,19	0,187	0,21	0,176	0,197	

As the first iteration of the calculation, the CB with fixed capacities (rated power) were installed in each node with load. Thus, the vector of CB conductivities $y(y_1, y_2, \dots, y_n)$ had $n=21$ variables.

Subsequently, as a result of set of solutions determination, some CB took zero values of the rated power.

The normalized vector of ranked CB conductivities y_{rank}^{nor} (marked by squares) is shown in Figure 1. It is similar to the

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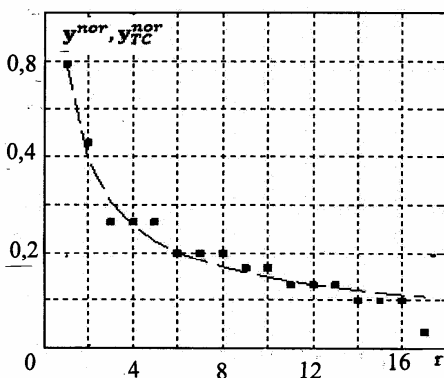


Fig. 1

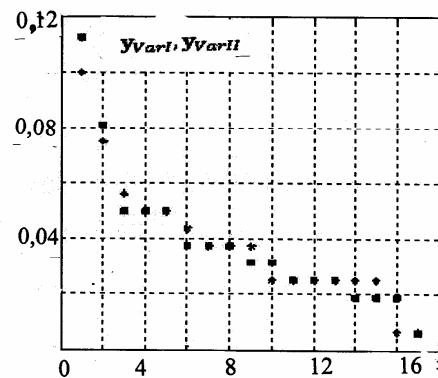


Fig. 2

normalized (approximated) vector in the form of a hyperbolic dependence y_{TC}^{nor} (marked by continuous line), which has a low value of first rank $y_{TC(r=1)}^{nor}=0,5919$ and rank factor $\beta=0,605$.

The comparison of CB reactive power QC for two variants respectively is based on the following criteria:

- Variant I: Criteria (1) and (2) are applied,
- Variant II: Criteria (1), (2) and (5) are applied.

The Figure 2 shows the target vector y of ranked CB conductivities (marked by squares), which is similar to normalized vector in the form of a hyperbolic dependence $y_{var I}$ for Variant I and vector $y_{var II}$ for Variant II (marked by asterisks), which corresponds to the minimum cost B_{min} after the corresponding conductivities ranking. These variants of CB placement and sizing are shown in Table II.

Table II

q	y, [p.u.]		q	y, [p.u.]		q	y, [p.u.]		q	y, [p.u.]	
	Criteria of Variant			Criteria of Variant			Criteria of Variant			Criteria of Variant	
	I	II		I	II		I	II		I	II
1	0	0	8	0,0375	0,0375	15	0	0	22	0,0063	0,0063
2	0	0	9	0	0	16	0,050	0,050	23	0,025	0,0187
3	0	0	10	0,0563	0,0500	17	0	0	24	0,025	0,025
4	0,0750	0,0813	11	0,100	0,1125	18	0,0438	0,050	25	0,025	0,0187
5	0	0	12	0	0	19	0,025	0,025	26	0,025	0,0313
6	0,0375	0,0313	13	0,050	0,0375	20	0	0	27	0,0063	0,0187
7	0	0	14	0,0375	0,0375	21	0,025	0,025	-	-	-

The results of CB selection by variants I and II are shown in Table III. In comparison with the case of Variant I, the active losses ΔP in the case of Variant II increased by 0,16% and the cost increased by 0,18%. When using TC-criterion in case of Variant II, the slight increase of cost allows to use this criterion for practical purpose of CB selection.

Table III

Applicable criteria	Criteria Of Var I	Criteria of Var II
Active losses (p.u.)	0,03131	0,03136
Cost B (usa/year)	197556	197907
Cost CB (usa)	3172	3274
Magnitude of conductivity of CB of the first rank $y_{(r=1)}$ [p.u.]	0,1	0,1125

In the Column 3 of Table IV the worst case of CB disconnection is presented. In this case the maximum quantity of nodes, with voltage deviation less than 0,95 p.u., was found. It is obvious that in the case of Variant II the result is better. All investigated negative voltage deviations was greater than value $U<0,92$.

The results show that the proposed combined algorithm (Variant II) allows to obtain the reduction of quantity of nodes with voltage deviation less than 0,95 p.u. in all cases of each one CB disconnection. At the same time active losses and cost slight increase. Combined algorithm is useful for practical purposes.

V. Conclusion. The combination of traditional criteria of yearly active losses and costs minimization with additional TC-criterion was proposed in order to obtain the specific solution for CB sizing and placement in RDN. The method of concessions was used to solve the multi-criteria problem in conjunction with PSO-method. The proposed algorithm allows to find the vector of ranked CB conductivities in correspondence with specific hyperbolic (power law) H -distribution according to the considered TC-approach.

Table IV				
1	2		3	
$U, [p.u.]$	The quantity of nodes with voltage deviation less than 0,95 p.u. in all cases of each one CB disconnection		The quantity of nodes with voltage deviation less than 0,95 p.u. in the worst case of one CB disconnection	
	Criteria of Var I	Criteria of Var II	Criteria of Var I	Criteria of Var II
$U<0,95$	100	82	19	15
$U<0,94$	23	19	12	8
$U<0,93$	6	2	6	2

In comparison with a traditional one, the application of the proposed algorithm allows to improve the voltage profile stabilization by decreasing the quantity of nodes with voltages,

which are out of permissible range when single capacitor bank is alternately disconnected. The results show that

proposed algorithm of CB placement and sizing in radial distribution networks can be quite effective for practical purposes.

1. AlHajri M., AlRashidi M. and El-Hawary M. A novel discrete particle swarm optimization algorithm for optimal capacitor placement and sizing / 2007 Proceedings of Canadian Conference on Electrical and Computer Engineering (CCECE). – 2007. – Pp. 1286-1289.
2. Gnatyuk V.I. The Law of Technocoenosis Optimum Construction. Vol.29. – Moskva: Publishing House of Tomsk State University, 2005. – 384 p. Available at: <http://gnatukvi.ru/ind.htm> (accessed 27.05.2015). (Rus)
3. Halil T., and Gorpnich A. Selection of Optimal Conductors Sections and Capacitors Placement in Radial Distribution Systems by Selective Particle Swarm Optimization // Scientific Papers of Donetsk National Technical University. – 2011. – Vol. 11. – Pp. 406-413. (Rus)
4. Kudrin B.I. Introduction to Technetics. – Moskva: Publishing House of Tomsk State University. – Pp. 1993-552. (Rus)
5. R2014b. Matlab Release. Available at: <http://www.mathworks.com/help/matlab/ref/sort.html> (accessed 27.05.2015).
6. Sirjani R., Mohamed A., Sharef H. Heuristic Optimization Techniques to Determine Optimal Capacitor Placement and Sizing in Radial Distribution Networks: A Comprehensive Review // Przegląd Elektrotechniczny (Electrical Review). – 2012. – No 7a. – Pp. 1-7.
7. Shi Y., and Eberhart R. A modified particle swarm optimizer / The 1998 IEEE International Conference on Evolutionary Computation Proceedings. – 1998. – Pp. 69–73.
8. Torres S.P., Castro C.A., Pringles R.M. Comparison of Particle Swarm Based Metaheuristics for the Electric Transmission Network Expansion Planning Problem // IEEE Power and Energy Society General Meeting. – 2011. – Pp. 1-7.
9. Vahid M., Hossein A.A., Kazem M. Maximum loss reduction applying combination of optimal conductor selection and capacitor placement in distribution systems with nonlinear loads / Universities Power Engineering Conference, 2008. UPEC 2008. 43rd International. – 2008. – Pp. 1–5.

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ВИБІР МІСЦЬ ВСТАНОВЛЕННЯ КОНДЕНСАТОРНИХ УСТАНОВОК У РАДІАЛЬНИХ РОЗПОДІЛЬНИХ МЕРЕЖАХ

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Для мінімізації електричних втрат, вартості електричних втрат та конденсаторних установок (КУ) представлено комбінований алгоритм для вибору потужності і місць розташування КУ у розподільних мережах із радіальною конфігурацією. У запропонованому алгоритмі використовуються метод поступок та модифікований PSO-метод. Додатково введено техноценологічний критерій: приналежність ранжованих змінних до класу нелінійних показових послідовностей. Запропонований підхід дозволяє отримувати ефективні практичні рішення та підвищену стабілізацію профілю напруги у радіальній розподільній мережі. Показано позитивні результати використання запропонованого алгоритму, зокрема зменшення кількості вузлів з напругою, нижчою за нижній поріг, у разі відключенні будь-якої КУ. Бібл. 9, табл. 4, рис. 2.

Ключові слова: конденсаторна установка, комбінований алгоритм, радіальна розподільна мережа, метод поступок, PSO-метод, техноценологічний критерій.

ВЫБОР МЕСТ УСТАНОВКИ КОНДЕНСАТОРНЫХ УСТАНОВОК В РАДИАЛЬНЫХ РАСПРЕДЕЛИТЕЛЬНЫХ СЕТЯХ

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Для минимизации электрических потерь, стоимости электрических потерь и конденсаторных установок (КУ) представлено комбинированный алгоритм для выбора мощности и мест расположения КУ в распределительных сетях с радиальной конфигурацией. В предложенном алгоритме используются метод уступок и модифицированный PSO-метод. Дополнительно введено техноценологический критерий: принадлежность ранжированных переменных к классу нелинейных показательных последовательностей. Предложенный подход позволяет получить эффективные практические решения и повышенную стабилизацию профиля напряжения в радиальной распределительной сети. Показаны положительные результаты использования предложенного алгоритма, в частности, уменьшение количества узлов с напряжением ниже нижнего порога, при отключении любой КУ. Библ. 9, табл. 4, рис. 2.

Ключевые слова: конденсаторная установка, комбинированный алгоритм, радиальная распределительная сеть, метод уступок, PSO-метод, техноценологический критерий.

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