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Anisotropy of ultrasonic waves propagation velocities in CdHgTe/CdTe

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Abstract.The complete set of elastic moduli of Cd_{0.2}Hg_{0.8}Te was obtained. Taking into account elastic moduli found for Cd_{0.2}Hg_{0.8}Te and appropriate literary data for CdTe the anisotropy of velocities of volume and Rayleigh waves propagating on (100) and (110) boundaries was calculated. Finally, peculiarities of the anisotropy of SAW propagating velocities for each of components of layered structures CdHgTe/CdTe and for the heteroepitaxial structure as a whole were analysed.

Keywords: II-VI semiconductors, ultrasound waves, anisotropy.

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1. Introduction

Variable band-gap CdHgTe semiconductors are known to be very important for use in infrared detection devices. It is also known that they are sensitive to external influences because the essential number of linear structural defects (dislocations, low angle boundaries, blocks boundaries, etc.) and low threshold of plasticity are especial properties of this type of alloys [1]. So, CdHgTe crystals are sensitive to high-frequency intensive ultrasound influence [2,3]. Taking into account wide applications of investigated materials in infrared engineering when using the form of heterostructure, there is the necessity in special research of surface acoustic properties. Such data are important both for the development of acoustic methods of improving of CdHgTe/CdTe layered structure parameters and for the development on its basis the novel acoustoelectronic devices with the acoustically controlled characteristics. So, the aim of this work was to study and compare the anisotropy of elastic properties of CdTe and $Cd_xHg_{1-x}Te$ (x = 0.2) semicon-ducting crystals.

2. Experiment

At room temperature, velocities of longitudinal (V_L) and transverse (V_{S1} , V_{S2}) ultrasonic waves propagating in <110> and <111> directions in the volume of p- Cd_{0.2}Hg_{0.8}Te samples were measured experimentally by phase-slope method [4] (f= 5–15 MHz, velocity error was less than 1–2 percents).

3. Results and discussion

3.1. Anisotropy of a sound velocity of volume waves

Taking into account elastic moduli obtained for $Cd_{0.21}Hg_{0.79}Te$ [5] and appropriate literary data for CdTe [6] (see Table), the anisotropy of velocities of bulk and Rayleigh waves, propagating in [110] direction and on (100) and (110) boundaries, were calculated according to [6].

Results of velocity calcualtions for ultrasonic waves in CdTe and Cd_{0.21}Hg_{0.79}Te crystals are presented in Figs 1,2; where V_L , V_{S1} , V_{S2} correspond to curves 1, 2, 3 for Cd_{0.21}Hg_{0.79}Te and curves 1°, 2°, 3° for CdTe. Let us mention that V_{S1} corresponds to the transvere wave S1 with preferable polarization in the direction perpendicular to the plane of the propagation. On the contrary, polarization of the transvere wave S2 with the velocity V_{S2} lies in the plane of the propagation. As one can see degeneration of transvere waves propagating along axes of the symmetry of third and fourth orders (directions <111> and <100>) takes place. In general, two transvere waves with defined co-perpendicular polarization can propagate in any crystal direction.

As it is shown by our calculations (Figs 1b, 2b), there are some directions in CdTe and Cd_{0.21}Hg_{0.79}Te crystals where velocities of the transverse wave are the same. For example, it occurs in the plane (100) for V_{S2} at $\varphi = 22^{\circ}$; in the plane (110) for V_{S1} at $\varphi = 47^{\circ}$ and for V_{S2} at $\varphi = 26^{\circ}$ and $\varphi = 64^{\circ}$. This fact could be used for the development of photoelectric matrix elements which use boundaries of materials, for example the heteroepitaxial CdHgTe/CdTe ones [7].

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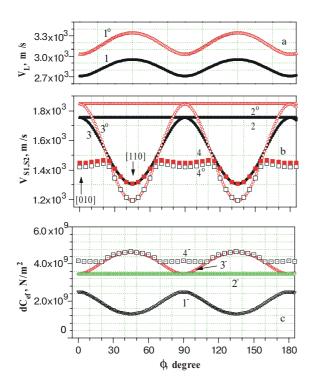


Fig. 1. Plane (100). Angle dependences of velocities V_L , longitudinal waves – curves 1, 2, 3 (a); V_{SI} , transverse wave with perpendicular polarization to the plane (100) – 2, 2°, 2°; V_{S2} , transverse wave with main polarization in the plane (100) – 3, 3°, 3°; V_R , – Rayleigh wave 4, 4°, 4° (b); differences of effective elastic moduli dC_{ef} (c). The curves 1, 2, 3, 4 correspond to $Cd_{0.21}Hg_{0.79}Te$, 1°, 2°, 3°, 4° – CdTe, 1°, 2°, 3°, 4° – Cd

3.2. Anisotropy of sound velocity of surface waves

Taking into account possible applications of CdHgTe/CdTe heteroepitaxial structures, it is necessary to analyze elastic properties of their boundary in detail. Such capabilities can be realized by surface acoustic wave (SAW) study. The SAW exists on a free surface of solids. These waves have a longitudinal displacement in the direction of the propagation as well as a transverse displacement in the perpendicular direction to the wave vector and the surface. Calculations of Rayleigh SAW velocities V_R were made by numeric methods [4] using computer. Values of elastic moduli used for calculations are shown in the table.

The results of the anisotropy of V_R in planes (100) and

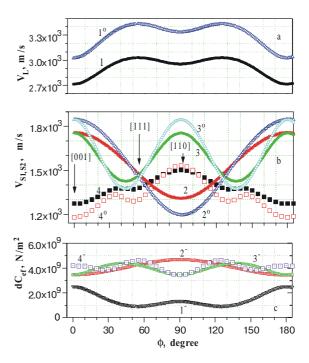


Fig. 2. Plane (110). Angle dependences of velocities V_L , longitudinal waves – curves 1, 2, 3 (a); V_{S1} , transverse wave with perpendicular polarization to the plane (110) – 2, 2°, 2°; V_{S2} , transverse wave with main polarization in the plane (110) – 3, 3°, 3°; V_R , – Rayleigh wave 4, 4°, 4° (b); differences of effective elastic moduli dC_{ef} (c). The curves 1, 2, 3, 4 correspond to $Cd_{0.21}Hg_{0.79}Te$, 1°, 2°, 3°, 4° – CdTe, 1°, 2°, 3°, 4° – Cd

(110) are given in Figs 1b and 2b, respectively (curves 4, 4°). Values of V_R for CdTe and Cd_{0.21}Hg_{0.79}Te in the plane (100) are different in any direction. But there is the special direction at $\varphi = 76^{\circ}$ in the plane (110) where velocities V_R of both materials are the same (1480 m/s). In our opinion, this crystallographic direction can be considered as the promi-sing one for the development of acoustical electronic devices based on CdHgTe/CdTe heteroepitaxial structures.

3.3. Surface elastic affinity of materials

Comparing effective elastic moduli of certain materials of such pairs we propose a new characteristic for evaluating capability of this layered structure components - surface elastic affi-

Table. Elastic moduli C_{ij} , Poisson coefficient $n = C_{12}/(C_{11} + C_{44})$ and density $Cd_xHg_{1-x}Te$ at 300 K.

Material	Elastic moduli, C_{ij} ,× 10^{10} Pa		Poisson coefficient	Density, 10^3 kg/m^3	References
	C ₁₁	C_{12} C_{44}	ν	ρ	
CdTe	5.351	3.681 1.994	0.408	5.86	[4]
<i>p</i> - Cd _{0.2} Hg _{0.8} Te	5.35	3.08 2.01	0.365	7.625	Our data
Cd _{0.21} Hg _{0.79} Te	5.6	3.0 2.34	0.349	7.603	[5]

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nity of materials (SEAM). It is supposed that the SEAM describes correctly a field of elastic stresses on the boundary of these environments, too. Parameters for a quantitative evaluation of SEAM can be chosen as $dC_{ef} = dC_R^{SL} = C_R^S - C_R^L$, where $C_R^{S,L} = (\rho^{S,L})(V_R^{S,L})^2$, and $V_R^{S,L}$ is the velocity of the propagation of a surface acoustic wave (the indexes S, L correspond to the substrate and the layer, accordingly). This parameter can be directly obtained from real elastic stresses on the boundary. Parameter dC_R^{SL} for Rayleigh waves and also dC_L^{SL} , dC_{S1}^{SL} , dC_{S2}^{SL} for two planes (100), (110) are presented in Figs 1c,2c (curves 4^- , 1^- , 2^- , 3^- , accordingly). As it is shown (Figs 1c,2c), the value of dC_R^{SL} was very close to dC_{S2}^{SL} . It signifies that dC_{S2}^{SL} can be selected as approximation the SEAM parameter since calculation of angular relation of dC_{S2}^{SL} is much easier than that of dC_R^{SL} .

Respective optimum versions for structures, geometry and orientation for different pairs of substrate and layer can be easily chosen using machine calculation of the anisotropy $dC^{S,L}$. Such method of selection can pursue various purposes. For example, $dC^{S,L}$ should be minimum for heteroepitaxial structure and, on the contrary, $dC^{S,L}$ should be maximum for nanostructures.

Conclusions

On the base of results obtained for CdHgTe and CdTe monocrystals an acoustic criterion of surface elastic affinity

for bordering layered structures is proposed, which, in accord with other physical reasons, sdefines the degree of mechanical stresses on the boundary of this sections.

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